## Applying the Water Quality Volume

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## Post-Construction Storm Water Mgmt.

"So that a receiving stream's physical, chemical and biological characteristics are protected, and stream functions are maintained, post-construction practices shall provide long-term management of runoff quality and quantity."


## 1. Effective BMP

Table 4a Extended Detention Post-Construction Practices with Minimum Drain Times

| Extended Detention Practices | Minimum Drain Time of WQv |
| :--- | :---: |
| Wet Extended Detention Basin ${ }^{1,2}$ | 24 hours |
| Constructed Extended Detention Wetland | 24 hours |
| Dry Extended Detention Basin | 48 hours |
| Permeable Pavement - Extended Detention | 24 hours |
| Underground Storage - Extended Detention | 24 hours |
| Sand $\&$ Other Media Filtration - Extended Detention <br> 5 | 24 hours |

Table 4b Infiltration Post-Construction Practices with Maximum Drain Times

| Infiltration Practices | Maximum Drain Time of WQv |
| :--- | :---: |
| Bioretention Area/Cell 1,2 | 24 hours |
| Infiltration Basin | 24 hours |
| Infiltration Trench ${ }^{2}$ | 48 hours |
| Permeable Pavement - Infiltration ${ }^{3}$ | 48 hours |
| Underground Storage - Infiltration ${ }^{3,4}$ | 48 hours |

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## 2. Water Quality Volume (WQv)

## $\mathrm{WQv}=\mathrm{P}_{\mathrm{wq}} \times \mathrm{Rv} \times \mathrm{A} \div 12$

WQv = water quality volume (ac-ft)
$P_{\text {wq }}=0.90$ inches
Rv = volumetric runoff coefficient
A = disturbed or contributing drainage area (acres)

## Runoff Coefficient $R \mathrm{v}=0.05+0.9$ (i)

- $\mathrm{i}=$ fraction impervious (impervious area $\div$ total area)
- Volumetric, not influenced by conditions such as intensity - Similar but not same as rational method coefficient "C"


## CALCULATION SCENARIOS

- New Construction
- Previously Developed Areas (Redevelopment)
- Water Quality Flow


## Example Site

Total site area:
Total disturbed area:
Planned impervious area:
2.25 acres
2.25 acres
1.35 acres

All WQv's will be shown in cubic feet

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## WQv Required

## $\mathrm{WQv}=\mathrm{P}_{\text {wq }} \times R \mathrm{Rv} \times \mathrm{A}_{\text {disturbed }} \div 12$ <br> $R v=0.05+0.9(i)$

Where:
$\mathrm{i}=1.35 \mathrm{ac} \div 2.25 \mathrm{ac}=0.60(60 \%)$
$R v=0.05+0.9(0.60)=0.59$
$P_{w q}=0.90 \mathrm{in}$


WQv (required) $=0.100$ ac-ft $\quad\left(4,337 \mathrm{ft}^{3}\right)$

## WQv Design

The site is required to treat $4,337 \mathrm{ft}^{3}$ with postconstruction BMPs; however each post-construction BMP must be designed to treat 100\% of the WQv for its contributing area.

The full 2.25 acre disturbance is graded toward a single post-construction BMP. In this case, the disturbed area and BMP drainage area are both 2.25 acres with Rv = 0.59:
$W Q v($ design $)=W Q v($ required $)=4,337 \mathrm{ft}^{3}$


## Offsite Run-on

An additional 0.75 acres runs onto the site from beyond the disturbance, draining to the post-construction BMP.

Unless diverted, the BMP design WQv must include this contributing drainage area.


## Offsite Run-on

$R v=0.05+0.9(i)$
$\mathrm{i}=1.35 \mathrm{ac} \div 3.00 \mathrm{ac}=0.45(45 \%)$
$R v=0.05+0.9(0.45)=0.455$
$W Q v=P_{\text {wq }} \times R v \times A_{\text {drained }} \div 12$
Where:
$P_{w q}=0.90$ in
Rv $=0.455$
$\mathrm{A}=3.00 \mathrm{ac}$
WQv (design) $=4,460 \mathrm{ft}^{3}$

## Multiple Drainage Areas

If the disturbed area contains separate drainage areas, each must have a post construction BMP sized to its contributing drainage area.

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## Multiple Drainage Areas

## Drainage Area \#1

Total area:
1.50 ac

68\%
Impervious:

$R v=0.05+0.9(0.68)=0.662$

Drainage Area \#2
Total area:
Impervious:
0.75 ac 44\%
$R v=0.05+0.9(0.44)=0.446$


## Multiple Drainage Areas

Drainage Area \#1
$W Q v=0.90$ in $\times 0.662 \times 1.50 \mathrm{ac} \div 12$
WQv (design) $=3,244 \mathrm{ft}^{3}$


Drainage Area \#2
WQv $=0.90$ in $\times 0.446 \times 0.75 \mathrm{ac} \div 12$
WQv (design) $=1,093 \mathrm{ft}^{3}$


WQv $($ design $)=3,244+1,093=4,337 \mathrm{ft}^{3}$

## Multiple Drainage Areas

Total area: $\quad 0.225$ ac Impervious: $\quad 27 \%$ $R v=0.05+0.9(0.27)=0.293$<br>$W Q v=0.9$ in $\times 0.293 \times 0.225 \div 12$ $W Q v=215 \mathrm{ft}^{3}$



## Minor Drainage Areas

## RRM using a grass filter strip or infiltration trench (to spec.):

| Runoff Reduction Practice | Impervious Cover <br> in Contributing <br> Drainage Area | Pervious Cover in <br> Contributing <br> Drainage Area | Volume <br> Received by <br> Practice |  |
| :--- | :---: | :---: | :---: | :---: |
|  | $\left(\mathrm{ft}^{2}\right)$ | $\left(\mathrm{ft}^{2}\right)$ | $\left(\mathrm{ft}^{3}\right)$ |  |
| Sheetflow to Grass Filter Strip with C/D Soils | 2644 | 7157 | 215 | fi |


| Disconnection <br> Area of Practice | Storage Volume <br> Provided by <br> Practice |
| :---: | :---: |
| $\left(\mathrm{ft}^{2}\right)$ | $\left(\mathrm{ft}^{3}\right)$ |
| 7157 | N/A |


| Runoff <br> Reduction <br> Volume | Remaining <br> Volume |
| :---: | :---: |
| $\left(\mathrm{ft}^{3}\right)$ | $\left(\mathrm{ft}^{3}\right)$ |
| 215 | 1 |


| Runoff Reduction Practice | Impervious Cover in Contributing Drainage Area | Pervious Cover in Contributing Drainage Area | Volume Received by Practice |
| :---: | :---: | :---: | :---: |
|  | ( $\mathrm{ft}^{2}$ ) | $\left(\mathrm{ft}^{2}\right)$ | $\left(\mathrm{ft}^{3}\right)$ |
| 7. Infiltration Practice |  |  |  |
| Infiltration Practice | 2644 | 7157 | 215 |


| Storage Volume <br> Provided by <br> Practice | Runoff <br> Reduction <br> Volume | Remaining <br> Volume |
| :---: | :---: | :---: |
|  | $\left(\mathrm{ft}^{3}\right)$ | $\left(\mathrm{ft}^{3}\right)$ |

## PREVIOUSLY DEVELOPED AREAS



## Options for Previously Developed Areas

1. Reduce the site Rv at least $20 \%$, or
2. Use a post-c BMP with the WQv from CGP equation 3:

$$
W Q v=\left[\left(0.2 \times R v_{1}\right)+\left(R v_{2}-R v_{1}\right)\right] \times P_{\text {wq }} \times A_{\text {dist }}
$$

Where:
$\mathrm{Rv}_{1}=$ Pre-development runoff coefficient $\mathrm{Ri}_{2}=$ Post-development runoff coefficient

> Existing site
> impervious $=77 \%$
> $\operatorname{Rv}_{1}=0.05+0.9(0.77)=0.743$

## 1. Decrease Rv $\geq 20 \%$

Proposed site

Rv decreases by 20\%, no additional BMP required
impervious = 60\%
$R \mathrm{v}_{2}=0.05+0.9(0.60)=0.590$
$(0.59 \div 0.743)-100 \%=\underline{21 \%}$ decrease Protection Agency

## 2. BMP w/ Decreased Rv

## Existing site <br> impervious $=66 \%$ <br> $R \mathrm{v}_{1}=0.05+0.9(0.66)=0.644$

Proposed site
impervious = 60\%
$R \mathrm{v}_{2}=0.05+0.9(0.60)=0.590$
$100 \%-(0.590 \div 0.644)=8.4 \%$ decrease /hio

## 2. BMP w/ Decreased Rv

A post construction BMP is required for the WQv as calculated:

$$
\begin{gathered}
\mathrm{WQv}=\left[\left(\mathrm{Rv}_{1} \times 0.2\right)+\left(\mathrm{Rv}_{2}-\mathrm{Rv}_{1}\right)\right] \times \mathrm{P}_{\mathrm{wq}} \times \mathrm{A}_{\text {dist }} \\
=[(0.644 \times 0.2)+(0.590-0.644)] \times 0.9 \mathrm{in} \times 2.25 \mathrm{ac} \\
\mathrm{WQv}(\text { required })=550 \mathrm{ft}^{3}
\end{gathered}
$$

## 2. BMP w/ Decreased Rv

The site is required to treat $550 \mathrm{ft}^{3}$ with postconstruction BMPs; however each postconstruction BMP must be designed to treat 100\% of the WQv for its contributing area. Place the BMP such that its drainage area* is equal to or greater than:

$$
\begin{aligned}
& \mathrm{A}_{\text {drainage }}=\frac{\mathrm{WQ}_{v}}{\mathrm{P}_{\mathrm{wq}} \times \mathrm{Rv}} \times \frac{12}{43,560} \\
& \frac{550 \mathrm{ft}^{3}}{0.9^{\prime \prime} \times 0.95} \times \frac{12}{43,560}=0.18 \mathrm{ac}
\end{aligned}
$$



## What if Rv will increase?

Existing site
impervious $=43 \%$
$\operatorname{Rv}_{1}=0.05+0.9(0.43)=0.437$
Proposed site
impervious $=60 \%$
$R \mathrm{v}_{2}=0.05+0.9(0.60)=0.590$
$(0.590 \div 0.437)-100 \%=35 \%$ increase

## What if Rv will increase?

Using CGP Equation 3 (weighted Rv):

$$
\begin{aligned}
& \mathrm{WQv}=\left[\left(\mathrm{Rv}_{1} \times 0.2\right)+\left(\mathrm{Rv}_{2}-\mathrm{Rv}_{1}\right)\right] \times \mathrm{P}_{\mathrm{wq}} \times \mathrm{A}_{\text {dist }} \\
& =[(0.437 \times 0.2)+(0.590-0.437)] \times 0.9 \mathrm{in} \times 2.25 \mathrm{ac}
\end{aligned}
$$

WQv (required) $=1,766 \mathrm{ft}^{3}$

## Rv Increases - Applied

The site is required to treat $1,766 \mathrm{ft}^{3}$ with postconstruction BMPs; however each postconstruction BMP must be designed to treat 100\% of the WQv for its contributing area. Place the BMP such that its drainage area* is equal to or greater than:

$$
\begin{aligned}
& \mathrm{A}_{\text {drainage }}=\frac{\mathrm{WQ} Q_{v}}{\mathrm{P}_{\mathrm{wq}} \times \mathrm{Rv}} \times \frac{12}{43,560} \\
& \frac{1,766 \mathrm{ft}^{3}}{0.9 \mathrm{in} \times 0.95} \times \frac{12}{43,560}=0.57 \mathrm{ac}
\end{aligned}
$$

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## What if I mix new and old ?


1.50 acre site w/ existing impervious will be joined to a 0.75 acre undeveloped site to form a singular development.

## What if I mix new and old?



Redevelopment
WQv $=\left[\left(R v_{1} \times 0.2\right)+\left(R v_{2}-R v_{1}\right)\right] \times 0.9$ in $\times 1.5 \mathrm{ac}$
Where:

$$
\begin{aligned}
& \mathrm{i}_{1}=0.97 \mathrm{ac} \div 1.50 \mathrm{ac}=0.63(64.5 \%) \\
& \operatorname{Rv}_{1}=0.05+0.9(0.60)=0.59 \\
& \mathrm{i}_{2}=1.02 \mathrm{ac} \div 1.50 \mathrm{ac}=0.66(68 \%) \\
& \operatorname{Rv}_{2}=0.05+0.9(0.60)=0.59
\end{aligned}
$$

$$
\text { WQv (required) }=771 \mathrm{ft}^{3}
$$

## What if I mix new and old ?



New Development

## WQv $=0.9$ in $\times R v \times 0.75$ ac $\div 12$

Where:
$\mathrm{i}=0.33 \mathrm{ac} \div 0.75 \mathrm{ac}=0.45 \quad(44 \%)$
Rv $=0.05+0.9(0.60)=0.59$
WQv (required) $=1,093 \mathrm{ft}^{3}$

## What if I mix new and old ?



WQv (required) $=$ $1,093 \mathrm{ft}^{3}+771 \mathrm{ft}^{3}=1,864 \mathrm{ft}^{3}$

## Water Quality Flow

Flow-through practices (hydrodynamic separators, media / cartridge filters, grass swales) that do not provide a significant detention volume must use the Water Quality Flow (WQF):

$$
\text { WQF }=C \times i \times A
$$

Where:
WQF = water quality discharge rate (cfs)
C = runoff coefficient for use with rational method for estimating peak discharge
i = rainfall intensity (in/hr)
A = drainage area (ac)

| Table 3-1. Runoff Coefficients for Rational Formula. ${ }^{(14)}$ |  |
| :---: | :---: |
| Type of Drainage Area | Runoff Coefficient, C* |
| Business: |  |
| Downtown areas | 0.70-0.95 |
| Neighborhood areas | 0.50-0.70 |
| Residential: |  |
| Single-family areas | 0.30-0.50 |
| Multi-units, detached | 0.40-0.60 |
| Multi-units, attached | 0.60-0.75 |
| Suburban | 0.25-0.40 |
| Apartment dwelling areas | 0.50-0.70 |
| Industrial: |  |
| Light areas | 0.50-0.80 |
| Heavy areas | 0.60-0.90 |
| Parks, cemeteries | 0.10-0.25 |
| Playgrounds | 0.20-0.40 |
| Railroad yard areas | 0.20-0.40 |
| Unimproved areas | 0.10-0.30 |
| Lawns: |  |
| Sandy soil, flat, 2\% | 0.05-0.10 |
| Sandy soil, average, 2-7\% | 0.10-0.15 |
| Sandy soil, steep, 7\% | 0.15-0.20 |
| Heavy soil, flat, 2\% | 0.13-0.17 |
| Heavy soil, average, 2-7\% | 0.18-0.22 |
| Heavy soil, steep, 7\% | 0.25-0.35 |
|  |  |
| Streets: |  |
| Asphaltic | 0.70-0.95 |
| Concrete | 0.80-0.95 |
| Brick | 0.70-0.85 |
| Drives and walks | 0.75-0.85 |
| Roofs | 0.75-0.95 |
| *Higher values are usually appropriate for steeply sloped areas and longer return periods because infiltration and other losses have a proportionally smaller effect on runoff in these cases. |  |

## WQF $=\mathbf{C} \times \mathrm{i} \times \mathrm{A}$

C - the runoff coefficient for use with rational method for estimating peak discharge.
14. American Society of Civil Engineers, 1960. Desian Manual for Storm Drainage, New York, NY.

| Residential: |  |
| :--- | :--- |
| Single-family areas | $0.30-0.50$ |
| Multi-units, detached | $0.40-0.60$ |
| Multi-units, attached | $0.60-0.75$ |
| Suburban | $0.25-0.40$ |
| Apartment dwelling areas | $0.50-0.70$ |
|  |  |

If not provided in MS4 drainage manual.

## Water Quality Flow

Rainfall intensity (i) is determined from an intensity-duration-frequency curve for an event.

- The intensity should be selected for a duration equal to the time of concentration (tc) of the drainage area.
- I-D curve for Water Quality Event is provided in tabular format in Appendix C of the CGP.
- Tc should utilize a velocity based equation for each flow condition encountered (sheet, shallow concentrated, pipe, open channel, etc.)
- If the total Tc is $<5$ minutes, a 5 minute duration should be used ${ }^{1}$
- Sub areas may yield larger peak discharges than then entire area and should be evaluated separately.?


## Time of Concentration $\left(\mathrm{t}_{\mathrm{c}}\right)$

WQF for the entire drainage area:

$50^{\prime}$ overland grass
26.7 min

60' overland pavement 300 ' pipe flow $410^{\prime}$ total
2.0 min
1.3 min
$\mathrm{Tc}=30$ minutes
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## Water Quality Flow

WQF for the entire drainage area:

$$
\text { WQF }=C \times i \times A
$$



Where:
$\mathrm{C}=0.85$ (commercial area)
$\mathrm{i}=1.01 \mathrm{in} / \mathrm{hr}$
$\mathrm{A}=2.25 \mathrm{ac}$
WQF $=0.85 \times 1.01 \mathrm{in} / \mathrm{hr} \times 2.25 \mathrm{ac}$ WQF $=1.93 \mathrm{cfs}$

## Time of Concentration $\left(\mathrm{t}_{\mathrm{c}}\right)$

WQF for the impervious sub-area:


| $0^{\prime} \quad$ overland grass | 0.0 min |
| :--- | :---: |
| $50^{\prime}$ overland pavement | 1.8 min |
| 420' pipe flow | $\mathbf{1 . 8 \mathrm { min }}$ |
| $470^{\prime}$ total | $\mathrm{Tc}=3.6$ minutes |



## Water Quality Flow

WQF for the impervious sub-area:

$$
\text { WQF }=C \times i \times A
$$



Where:
$\mathrm{C}=0.90$ (impervious, flat)
$\mathrm{i}=2.37 \mathrm{in} / \mathrm{hr}$
$\mathrm{A}=1.35 \mathrm{ac}$
WQF $=0.90 \times 2.37 \mathrm{in} / \mathrm{hr} \times 1.35 \mathrm{ac}$
WQF $=2.88 \mathrm{cfs}$

## Water Quality Flow - Redevelopment

From our previous redevelopment example:
The site is required to treat $1,766 \mathrm{ft}^{3}$ with postconstruction BMPs; however each postconstruction BMP must be designed to treat 100\% of the WQv for its contributing area. Place the BMP such that its drainage area* is equal to or greater than:

$$
\begin{aligned}
& \mathrm{A}_{\text {drainage }}=\frac{\mathrm{WQ}_{\mathrm{v}}}{\mathrm{P}_{\mathrm{wq}} \times \mathrm{Rv}} \times \frac{12}{43,560} \\
& \frac{1,766 \mathrm{ft}^{3}}{0.9 \mathrm{in} \times 0.95} \times \frac{12}{43,560}=0.57 \mathrm{ac}
\end{aligned}
$$

[^1]

## Water Quality Flow - Redevelopment

$$
\text { WQF }=C \times i \times A
$$

Where:
$C=0.90$
$\mathrm{i}=2.37 \mathrm{in} / \mathrm{hr}[\mathrm{tc}=3.3 \mathrm{~min}$.]
$\mathrm{A}=0.57 \mathrm{ac}$
$\mathrm{WQF}=0.90 \times 2.37 \mathrm{in} / \mathrm{hr} \times 0.57 \mathrm{ac}$
$W Q F=1.22 \mathrm{cfs}$


## Storm Water Technical Assistance

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[^0]:    * Should be highest expected pollutant load area

[^1]:    * Should be highest expected pollutant load area

